

REPORT DOCUMENTATION PAGE

Form Approved
OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.

1. AGENCY USE ONLY (Leave blank)		2. REPORT DATE 9/30/96	3. REPORT TYPE AND DATES COVERED Final Report; 10/01/91 - 02/28/96	
4. TITLE AND SUBTITLE Measurements of Turbulent Wall Eddies with Selective Suction			5. FUNDING NUMBERS \$109,489	
6. AUTHOR(S) Ron Blackwelder				
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Department of Aerospace Engineering University of Southern California Los Angeles, CA 90089-1191			8. PERFORMING ORGANIZATION REPORT NUMBER	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) Dr. Pat Purtell, Code 333 Office of Naval Research Ballston Tower One 800 North Quincy Street Arlington, VA 22217-5660			10. SPONSORING/MONITORING AGENCY REPORT NUMBER	
11. SUPPLEMENTARY NOTES				
12a. DISTRIBUTION / AVAILABILITY STATEMENT Approved for public release; distribution unlimited			12b. DISTRIBUTION CODE	
13. ABSTRACT (Maximum 200 words) See enclosed.				
14. SUBJECT TERMS turbulence, vortices, boundary layer			15. NUMBER OF PAGES 2	
			16. PRICE CODE	
17. SECURITY CLASSIFICATION OF REPORT Unclassified	18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified	19. SECURITY CLASSIFICATION OF ABSTRACT Unclassified	20. LIMITATION OF ABSTRACT UL	

19961015 003

GENERAL INSTRUCTIONS FOR COMPLETING SF 298

The Report Documentation Page (RDP) is used in announcing and cataloging reports. It is important that this information be consistent with the rest of the report, particularly the cover and title page. Instructions for filling in each block of the form follow. It is important to *stay within the lines* to meet optical scanning requirements.

Block 1. Agency Use Only (Leave blank).

Block 2. Report Date. Full publication date including day, month, and year, if available (e.g. 1 Jan 88). Must cite at least the year.

Block 3. Type of Report and Dates Covered. State whether report is interim, final, etc. If applicable, enter inclusive report dates (e.g. 10 Jun 87 - 30 Jun 88).

Block 4. Title and Subtitle. A title is taken from the part of the report that provides the most meaningful and complete information. When a report is prepared in more than one volume, repeat the primary title, add volume number, and include subtitle for the specific volume. On classified documents enter the title classification in parentheses.

Block 5. Funding Numbers. To include contract and grant numbers; may include program element number(s), project number(s), task number(s), and work unit number(s). Use the following labels:

C - Contract	PR - Project
G - Grant	TA - Task
PE - Program Element	WU - Work Unit Accession No.

Block 6. Author(s). Name(s) of person(s) responsible for writing the report, performing the research, or credited with the content of the report. If editor or compiler, this should follow the name(s).

Block 7. Performing Organization Name(s) and Address(es). Self-explanatory.

Block 8. Performing Organization Report Number. Enter the unique alphanumeric report number(s) assigned by the organization performing the report.

Block 9. Sponsoring/Monitoring Agency Name(s) and Address(es). Self-explanatory.

Block 10. Sponsoring/Monitoring Agency Report Number. (If known)

Block 11. Supplementary Notes. Enter information not included elsewhere such as: Prepared in cooperation with...; Trans. of...; To be published in.... When a report is revised, include a statement whether the new report supersedes or supplements the older report.

Block 12a. Distribution/Availability Statement. Denotes public availability or limitations. Cite any availability to the public. Enter additional limitations or special markings in all capitals (e.g. NOFORN, REL, ITAR).

DOD - See DoDD 5230.24, "Distribution Statements on Technical Documents."

DOE - See authorities.

NASA - See Handbook NHB 2200.2.

NTIS - Leave blank.

Block 12b. Distribution Code.

DOD - Leave blank.

DOE - Enter DOE distribution categories from the Standard Distribution for Unclassified Scientific and Technical Reports.

NASA - Leave blank.

NTIS - Leave blank.

Block 13. Abstract. Include a brief (*Maximum 200 words*) factual summary of the most significant information contained in the report.

Block 14. Subject Terms. Keywords or phrases identifying major subjects in the report.

Block 15. Number of Pages. Enter the total number of pages.

Block 16. Price Code. Enter appropriate price code (*NTIS only*).

Blocks 17. - 19. Security Classifications. Self-explanatory. Enter U.S. Security Classification in accordance with U.S. Security Regulations (i.e., UNCLASSIFIED). If form contains classified information, stamp classification on the top and bottom of the page.

Block 20. Limitation of Abstract. This block must be completed to assign a limitation to the abstract. Enter either UL (unlimited) or SAR (same as report). An entry in this block is necessary if the abstract is to be limited. If blank, the abstract is assumed to be unlimited.

Final Technical Report

"Measurements of Turbulent Wall Eddies with Selective Suction" (ASSERT) (N00014-92-J-1062)

10/01/91 to 02/28/96

by

Ron Blackwelder, Principal Investigator
Department of Aerospace Engineering
University of Southern California
Los Angeles, CA 90089-1191

Scientific Officer: Dr. Pat Purtell

Description of the Scientific Research Goals

This investigation was designed to aid the underlying research contract by providing flow visualization of the flow actuators used to control streamwise vortices in the wall region of a bounded shear flow.

Significant Results

The flow visualizations were performed in the USC Water Channel on a flat plate. The test section is 6m long and has a cross section of .6m x .9m. The turbulence intensity is less than 0.1% and provides an excellent test bed for transition and turbulent studies. The results have illustrated a different mechanism for producing low speed regions and streamwise vortices near the wall. The experimental setup was similar to that used in the wind tunnel in the associated report. Fixed and active delta wing actuators were used. They were scaled to the flow parameters in the laminar boundary layer in the water channel. The non-dimensional frequencies were similar to those used in the wind tunnel. However when the actuators were implemented, vortices of the opposite sign and an order of magnitude larger than expected were generated as discussed below.

Vortex generators consisting of small fixed delta wings with amplitudes of typically a quarter of the boundary layer thickness were placed on the wall of the water channel. When a delta wing had its apex pointed upstream, the two vortices which were produced had a down-flow between them. The visualization showed that these vortices were very stable and the vortices persisted for great distances (typically a hundred boundary layer thickness) downstream. This resulted from the mutual interaction of the vortices; i.e. the induced flow causes them to move apart from each other in the spanwise direction thus decreasing their interaction. On the other hand, when a delta wing was placed into the flow field with its apex pointed downstream, the two counter-rotating vortices which are produced have a mutual interaction that attracts them to each other and they interact. This produces

an up-flow between them; i.e. the normal velocity is positive between the two vortices, and they move away from the wall. These vortices were very unstable and persisted only a few boundary layer thickness downstream. Consequentially, when fixed delta wings are used as vortex generators, they should be designed with the above results in mind.

When the piezo-ceramic delta wings were flush mounted on the wall and oscillated, a completely different phenomena was observed which illuminated how the actuators are able to delay the transition. Initially it was assumed that the oscillating delta wing would produce unsteady vortices that would counteract the existing streamwise Görtler vortices. However it was discovered that when the actuator was orientated to produce such vortices, the transition was hastened. The visualization indicated the reason. First, since very small amplitudes (i.e. of the order of v/u_τ) produced large effects, the delta wings were operating in a strongly viscous region and hence no discernable vortices were produced. Instead the high frequency oscillations of the delta wing (which is approximately parallel to the wall) produced a streaming flow parallel to the wall. The actual direction depended upon the geometry of the actuator. For the delta wing, a strong spanwise component was evident. This component created a spanwise streaming flow very near the wall that moved in the spanwise direction until slowed by viscosity. This displaced fluid accumulated at a fixed spanwise location depending upon the frequency, amplitude and geometry of the actuator. As more fluid was displaced in the spanwise direction, the accumulated fluid moved upward and convection carried it downstream. With continued oscillation, the net result was a new region of low speed fluid which corresponded to a large scale steady pair of counter-rotating vortices. However, their sense of rotation was opposite to the steady state vortices discussed above. This region was 180° out of phase from where it would be expected if the wing were shedding streamwise vortices.

This phenomena disclosed a new method of generating streamwise vortices that may have several advantages. First, when the device was not in use, it was flush with the wall with no protrusions. Secondly, to generate a low speed region comparable to that produced by a fixed delta wing required an amplitude at the apex of the delta wing an order of magnitude lower than the amplitude of the steady state delta wing described above. Thirdly, the lower amplitude implied that the device drag should be much lower than the device drag of the steady state vortex. Although the drag produced by these devices has not yet been measured, it is expected to be significantly lower than that of the steady state delta wing because their amplitudes are an order of magnitude smaller. Fourthly, they produce a significant spanwise velocity at the wall which could be significant in reducing the drag in turbulent bounded flows as has been demonstrated in the literature (i.e. Choi et al, JFM, 262, 75, 1994).